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# A Model of Motor and Sensory Axon Activation in the Median Nerve Using Surface Electrical Stimulation

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## ABSTRACT

Surface electrical stimulation has the potential to be a powerful and non-invasive treatment for a variety of medical conditions but currently it is difficult to obtain consistent evoked responses. A viable clinical system must be able to adapt to variations in individuals to produce repeatable results. To more fully study the effect of these variations without performing exhaustive testing on human subjects, a system of computer models was created to predict motor and sensory axon activation in the median nerve due to surface electrical stimulation at the elbow. An anatomically-based finite element model of the arm was built to accurately predict voltages resulting from surface electrical stimulation. In addition, two axon models were developed based on previously published models to incorporate physiological differences between sensory and motor axons. This resulted in axon models that could reproduce experimental results for conduction velocity, strength-duration curves and activation threshold. Differences in experimentally obtained action potential shape between the motor and sensory axons were reflected in the models. The models predicted a lower threshold for sensory axons than motor axons of the same diameter, allowing a range of sensory axons to be activated before any motor axons. This system of models will be a useful tool for development of surface electrical stimulation as a method to target specific neural functions.

Keywords – Axon model; Motor axon model; Sensory axon model; Finite element model; Surface electrical stimulation

## **1** INTRODUCTION

Surface electrical stimulation has the potential to be a powerful and non-invasive treatment for a variety of medical conditions. Electrical stimulation in general is used to promote plasticity and recovery of voluntary movements in individuals with spinal cord injury (Angeli et al. 2014) and stroke (Peurala et al. 2002; Walker et al. 2014). Treatments involving electrical stimulation are also being developed for conditions such as diabetes, asthma, hypertension, arthritis, pain and cancer (Birmingham et al. 2014). Surface electrical stimulation as a method to target specific neural functions would make such treatments more accessible and acceptable to patients.

Consistent responses are difficult to obtain using surface electrical stimulation due to variable electrode placement, skin movement and physiological variables that affect tissue conductance. A viable clinical system must be able to adapt to these variations to produce repeatable results. To more fully study the effect of these variations without performing exhaustive testing on human subjects, a set of computer models were developed. The models will facilitate prediction of the effect of different variables such as size, shape and location of electrodes on axon activation. Initially it will be used to develop an electrode array to be used in a therapy for treating phantom limb pain. The therapy will involve activating sensation by stimulating the median nerve at the elbow. This paper presents a set of models to predict the behavior of this application. The models were based on previous models published in literature (Howells et al. 2012; C. McIntyre et al. 2002; Schiefer et al. 2008) and validated with experimental data.

Modeling the activation of neurons using electrical stimulation involves performing two separate sets of calculations (Goffredo et al. 2014): 1) find the electric potentials due to the applied stimulation and 2) determine the effect of those potentials on the neuron (i.e. does it fire or not). Early modeling studies estimated potentials along the nerve due to a point source electrode in a homogeneous, isotropic medium near the nerve (W. Grill and Mortimer 1997; Warman et al. 1992). This method assumed that the electrode was sufficiently close to the axons that the extracellular space could be assumed to be homogenous. When the electrode is farther from the axon, this

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the tissue layers around the electrodes and nerve, each layer with distinct electrical properties. A simplified FE model of the arm that consisted of concentric cylinders of bone, muscle, fat and skin has been used predict responses due to transcutaneous electrical stimulation (Goffredo et al. 2014; Kuhn et al. 2009). However, this level of detail was not sufficient for the investigation of varying electrode arrangements. Schiefer et al developed a more detailed finite element model of extraneural stimulation that used actual human nerve cross sections to define the geometry (Schiefer et al. 2008). This model included an accurate rendition of the electrode as well as detailed neural features, such as the perineurim and epineurium. The purpose of the current study was to create a more detailed, whole-arm model that will allow investigation of changes in electrode position/arrangement.

There are many reported differences between motor and sensory axons, such as the fact that sensory axons have a lower threshold, a slightly higher conduction velocity and different recovery than motor axons (Dawson 1956; Forst et al. 2015; Kiernan et al. 1996). This study focused on the median nerve, which contains both motor and sensory fibers, so it was important to take into account these differences when predicting activation. These differences have been reported to be due to disparities in the properties of ion channels in the membrane (Bostock and Rothwell 1997; Howells et al. 2012). Many groups have developed individual motor or sensory models (Bostock et al. 1991; C. McIntyre et al. 2002; Wesselink et al. 1999), but in order to compare activation between the two types of axons, the models needed to be developed in concert, as was done by Howells et al (Howells model).

The Howells models included a single node and internode, similar to what is accessed during a space-clamped measurement. This allowed parameter development based on experimental results but cannot be used with voltages from the larger arm model. This model focused on the hyperpolarization-activated cyclic-nucleotide-gated (HCN) family of channels but also included different types of sodium and potassium channels at the node than in the internodal segments. In comparing motor and sensory axons, this study found that differences in channel gating parameters were at least as important as channel expression differences in explaining excitability differences (Howells et al. 2012). A double-cable mammalian motor axon model developed by McIntyre, Richardson and Grill (MRG model) (C. McIntyre et al. 2002) used the voltages along the axon to predict activation and therefore could be used with the larger arm model. The MRG model has been used for neural predictions in a variety of applications such as peripheral nerve activation (Peterson et al. 2011; Schiefer et al. 2008; Wongsarnpigoon et al. 2010), high frequency stimulation (Kilgore and Bhadra 2004; Medina and Grill 2016; Miles et al. 2007), and cortical activation (C. C. McIntyre and Grill 2002).

In this study, the benefits of these two models were combined; the MRG model was used as the foundation of a full axon model, and was modified to include ion channels used by Howells in the node and internode to produce new sensory and motor axon models. These models in combination with the whole arm model, could predict responses from surface electrical stimulation. The goal of this study was to verify model predictions with previously published experimental data to allow future investigation of variations in electrode arrangement.

## 2 METHODS

To fully model surface electrical stimulation, three models were developed. The first was a 3-dimensional, anatomically-based finite element method (FEM) model of the arm that included electrodes near the elbow and electrical properties for each tissue domain. This arm model was used to predict voltages in throughout the fascicles within the median nerve. The voltages were then applied to an axon model, which was created and run in NEURON (v7.3, (Hines and Carnevale 1997)) to predict whether or not a sensory or motor axon would fire in that particular location. Simulations were performed to predict what percentage of each type of axon were activated using different stimulation voltages and these results were validated with experimental data.

#### 2.1 Arm Model

Cross sections of the human arm were needed to represent the 3D structures of the arm. Simplified cross sections of the arm near the elbow were used that included the humerus, radius and ulna as well as muscles, blood vessels and nerves (Fig. 1) ("Elbow Cross Sectional Anatomy" 2014). Increasing the number of cross sections greatly

increased the complexity and solution time of the model so only two cross sections were used, one located at the elbow's synovial hinge joint and one 20 mm proximal to the joint. These locations were chosen to adequately represent the anatomy at the area where the electrodes were placed. The cross sections were traced using Creo Parametric (formerly Pro-Engineer from PTC, Akron, OH) then each tissue was swept along a trajectory between the two cross-sections placed 20mm apart. The ends were extruded 300 mm in each direction to minimize edge effects and approximately represent the length of the arm (Drillis et al. 1964).

The three dimensional assembly was imported into Maxwell 2014 (ANSYS, Canonsburg, Pennsylvania). Conductivity values were assigned to each tissue (Table 1). Two electrodes (17mm x 45 mm) were placed on the center of the arm to match experimental positioning (Forst et al. 2015) (Fig. 1).

ELECTRICAL PROPERTIES OF TISSUES				
Material	Conductivity (S/m)			
Epineurium	0.083 <sup>a</sup>			
Perineurium	0.002 <sup>a, d</sup>			
Endoneurium (longitudinal)	0.57 <sup>a, e</sup>			
Endoneurium (transverse)	0.08 <sup>a, e</sup>			
Blood	0.606 <sup>b</sup>			
Bone	0.02 <sup>c</sup>			
Fat	0.0303 <sup>c</sup>			
Muscle (longitudinal)	0.33 <sup>c</sup>			
Muscle (transverse)	0.11 <sup>c</sup>			
Skin	0.0014 <sup>c</sup>			
Tendon	0.06 <sup>f</sup>			

TABLE 1 ELECTRICAL PROPERTIES OF TISSUES

<sup>a</sup>(Choi et al. 2001), <sup>b</sup>(Geddes and Baker 1967), <sup>c</sup>(Kuhn et al. 2009),

<sup>d</sup>(Weerasuriya et al. 1984), <sup>e</sup>(Ranck and BeMent 1965), <sup>f</sup>(Dimbylow 2000)

There were four versions of the model, varying only in the anatomy of the median nerve. The first had a simplified nerve with a single fascicle (Fig. 2A) and was used to test parameters of the motor and sensory axon models as described below. The other three versions contained a random arrangement of fascicles, created to account for variations in human anatomy. The number of fascicles in a median nerve according to histological data ranges from 3 to 37, varying with location along the arm and among people (Sunderland 1978). For this study, ten fascicles were used. The fascicle diameters were based on measurements of a human median nerve cross-section at the elbow and ranged in diameter between 0.264 mm and 0.800 mm (Suresh et al. 2006). For each fascicle, the thickness of the perineurium was set to three percent of the fascicle diameter (Grinberg et al. 2008).

Stimulation was applied by setting the cathode (proximal electrode) to -1V and the anode to 1V. The boundary conditions of the ends of the model were set as ground (Schiefer et al. 2008). Frequency-independent simulations were performed using the DC Conduction solver in Ansys Maxwell. Auto-adaptive mesh refinement was used to generate a final mesh with a percent error in the voltage field of less than 0.05%. The voltages in the nerve along the length of the arm were exported to MATLAB R2013a (Mathworks, Natick MA) with a 0.05 mm resolution in the x-y directions and a 0.667 mm resolution in the z direction along the nerve (Fig. 1). The voltage changed smoothly throughout a single tissue so a lower resolution could be used along the nerve (z direction). In the X-Y plane, the largest error occurred with axons located near the edge of a fascicle and interpolation was performed between a point inside and outside the fascicle. For this reason, axons were not placed within one resolution distance from the edge of a fascicle (or 0.05 mm). This resolution resulted in 6 points across the smallest fascicle and 17 points across the largest fascicle.

#### 2.2 Axon Models

To predict the activation of sensory axons and address the differences between motor and sensory axons, new axon models were developed. The new models were based on a motor axon model (MRG model) (C. McIntyre et al. 2002) and created in the NEURON programming environment (Hines and Carnevale 1997). The MRG model was a double-cable model consisting of nodes separated by internodal segments coated in myelin. The internode was divided into ten segments: two paranodal myelin attachment segments (MYSA); two paranodal main segments (FLUT); and six internodal segments (STIN) (Fig. 3A). The major changes between the MRG model and the new models were the inclusion of a fast K<sup>+</sup> channel in the node and the addition of several channels in the internode as suggested by the Howells model (Howells et al. 2012). The MRG model lumped all internodal channels into a single conductance. The models developed here included fast K<sup>+</sup>, slow K<sup>+</sup>, leak, and hyperpolarization-activated cyclic-nucleotide gated (HCN) channels in the internode (Fig. 3B).

For the motor axon model, parameters used in the MRG model were retained when possible. Gating parameters from the Howells model were used to add HCN channel to the new model. The fast K<sup>+</sup> conductance in the node was found using the ratio of fast to slow potassium channels found in the Howells model. Ratios of the conductance of fast K<sup>+</sup>, slow K<sup>+</sup>, and leak between the node and internode reported by Röper and Schwarz (Roper and Schwarz 1989) were used to estimate the conductance values of the internode; however, the ratio between leak conductance of MYSA and that of FLUT and STIN was maintained from the MRG model. Reversal potentials were made to match the MRG model where possible. For the HCN channel, reversal potentials were calculated using the Goldman-Hodgkin-Katz equation using the concentrations and permeabilities reported in Howells.

The revised motor axon model was used as a foundation for the development of a sensory axon model. Each of the values used to calculate the gating parameters was converted from motor to sensory using the ratio found between these channels in the models by Howells (Howells et al. 2012). When possible, the internodal conductance values were derived using the ratios of internodal to nodal values found in Röper and Schwarz (Roper and Schwarz 1989). The ratio between the leak conductance of MYSA and that of FLUT and STIN was maintained from the MRG model. A value for the conductance per unit area of the HCN channel could not be found in literature for motor or sensory axons, so a range of values were tested, maintaining the motor-to-sensory ratio between the HCN absolute conductance values found in the Howells model. The values chosen were found to result in steady-state voltages close to the resting potentials given by the Howells model. At completion, the resting potential was -85.91 mV for the motor axon model and -79.37 mV for the sensory axon model compared to -84.4 mV and -80.3 mV from the Howells model. A table of parameter values can be found in Appendix B.

Validation of both axon models was performed using simulations of one axon centered in the single fascicle nerve model (Fig. 2A). This reduced the variability that would have resulted from randomizing axon location. Conduction velocity, action potential shape, and the strength-duration relationship were used to evaluate the model. A sensitivity analysis was conducted to determine the relative effects of each conductance parameter on the activation threshold. A fractional factorial design of type 2<sub>IV</sub><sup>11-6</sup> was used to separate the main effects of each parameter from the effects due to two-factor interactions. This involved 11 factors with two levels each and would require 2048 observations to do a full factorial design. The fractional design made it impossible to distinguish interactions of 3-factors or more but provided a statistical comparison of sensitivity with only 32 observations. The activation threshold was found with parameter combinations at two levels: the nominal value and double the nominal value. These thresholds were analyzed to determine the main effects of each parameter and all twofactor interaction effects. The tests were repeated with the parameters at the nominal value and half of the nominal value. While not ideal, this allowed a further exploration of the sensitivity of the model to decreasing the parameters without the nearly 200,000 observations required for a three level, 11 factor, factorial design.

#### 2.3 Simulation details

The calculated voltages within the more realistic ten fascicular nerves (Fig. 2C-E) were used to predict firing using the validated motor and sensory axon models. An axon length of 160 nodes (130 distal to the center of the cathode and 30 proximal) was found to accurately reproduce the results of using the full 620 mm length. Axons were randomly placed within each fascicle leaving 0.05 mm between the placement and the edge of the fascicle to avoid interpolation involving points in the perineurium. The diameter of axons was assigned randomly based on the reported distribution of diameters in the median nerve at the elbow (Fig. 4) (Buchthal and Rosenfalck 1966). Additionally, 15% of the 250 axons within each fascicle were randomly designated as motor axons. This is based on reports that 33% of axons in the median nerve were traced to muscles (Sunderland 1978) and 40%-60% of this 33% were estimated to be

efferent, motor axons (Ian A Boyd and Davey 1968; Feinstein et al. 1955). A pulse duration of 100 µs was used for all trials while the pulse amplitude was varied.

To find the whole nerve activation, the percent activation in each fascicle was weighted by the area and summed. This nerve activation was averaged across all three multi-fascicular versions of the model to compare motor and sensory axon activation and activation by diameter. To compare activation across the nerve, activation was averaged across all axon diameters and both axon types for each fascicle.

Statistical analysis was performed using R to quantify the effect of voltage, axon diameter, axon type, fascicular diameter and distance from the electrode on percent activation. After finding valid linear relationships, two linear regressions were performed. The first predicted percent activation of the entire nerve based on voltage, axon diameter, and axon type. The second predicted percent activation of a fascicle based on voltage, distance from the electrode, and fascicle diameter. Each regression was used to evaluate overall effectiveness by using the R<sup>2</sup> value, statistical significance of each factor by using an ANOVA test, and the presence of multi-variable interaction effects.

## **3 RESULTS**

The Maxwell arm model with the single fascicular nerve had 641,949 tetrahedra and required 5 hours to calculate the solution on a Windows 8.1 computer with a quad core, 3.4GHz processor. With the multi-fascicular nerve, there were 3,402,877 tetrahedra and 9 hours were required to calculate the solution. The NEURON models required about 40 seconds per axon to determine if that axon was activated for each location within the nerve and stimulation voltage.

#### 3.1 Single Axon Model

#### 3.1.1 Threshold Comparison

With the added channels and modified parameters, the sensory axon model predicted a lower threshold for a given fiber diameter than the motor axon model, as seen in Fig. 5. The shape of both curves is consistent with the fact that larger axons have a lower threshold. Additionally, the model predicted that sensory axons as small as 12  $\mu$ m could be activated at a lower voltage than 16  $\mu$ m diameter motor axons in the

same position. This would explain why sensations in the hand were reported without visible muscle contraction (Forst et al. 2015).

#### 3.1.2 Validation

Conduction velocity, strength-duration curves, and action potential shape from the new models matched experimental results reported in the literature. Conduction velocity was found to have a linear relationship with fiber diameter (Fig. 6). The slope of this relationship and the range of values from the models matched the experimental range measured in cats when adjusted for shrinkage of the experimental data (I A Boyd and Kalu 1979). Additionally, the conduction velocities predicted by the models for motor axons were slightly higher than sensory axons for a given fiber diameter, which is consistent with human experimental data (Dawson 1956).

Strength-duration curves from both sensory and motor axon models compared well with curves measured from human median and ulnar nerves (Panizza et al. 1994) for sensory and motor axons. When normalized to the rheobase voltage, the model data had a similar shape to curves produced experimentally for each type of axon (Fig. 7). For the 10  $\mu$ m fiber, the sensory axon model had a rheobase of 6.2V and a chronaxie of 0.23 ms. The motor axon model had a rheobase of 14.2 V and a chronaxie of 0.15 ms.

Differences were found between the shapes of the motor and sensory action potentials (Fig. 8) that matched differences seen in experimental recordings (David et al. 1995; Stebbing et al. 1999). The sensory model contained a much larger early hyperpolarization than motor that then rose gradually back to resting potential. The membrane voltage in the motor model instead stayed above resting potential immediately following the action potential, before it gradually decreased into hyperpolarization. The action potential also had a slightly longer duration in the motor model than the sensory, which was also found in the experimental voltage traces.

Although the simulated action potentials had a similar shape to experimental recordings, there were some differences in the timing of the action potential and the magnitude of the voltage fluctuations, especially during the afterpotential. The voltage during the afterpotential did go through periods of hyperpolarization and depolarization but this phase had a shorter duration and lower magnitude than seen experimentally.

The model action potentials were also narrower than the experimental recordings for both types of axons. The width of the action potential of the motor axon model was similar to that of the original MRG model but again there were differences in the timing and voltage magnitude during the afterpotential.

#### 3.1.3 Sensitivity Analysis

A sensitivity analysis was used to rank the importance of the contribution of each channel conductance to the activation threshold of the axon models (detailed list of parameters in Fig. 9). The difference between the average threshold of trials when each parameter was at double its nominal value and at its nominal value is shown in Fig. 9. Only the main effects are shown since the two-factor interactions were extremely small when compared with the main effects (< 0.6 V or <3.3% of threshold) and were considered negligible. The parameter with the largest effect on threshold was the fast sodium channel conductance (E in Fig. 9) followed by the conductance of the HCN channel and leak conductance (the top five contributors are bolded in the legend). The analysis of the parameters at the nominal values and half of the nominal values yielded similar results with the same top-five contributors. The details of the justification for the values chosen for these five parameters are in the discussion.

#### 3.2 Whole Nerve Activation

The actual distribution of axon diameters that resulted from the random assignment of axon diameters followed the intended distribution (data points in Figure 4). When the new axon models were used in the 10 fascicular nerves, sensory axons were again found to have a lower threshold than motor axons. For example, at 25 V, an average of 37% of sensory axons in the nerve were activated, while an average of 3% of motor axons were activated (Fig. 10A). This is consistent with experimental results where sensory percepts could be evoked without visible muscle contraction (Forst et al. 2015; Veale et al. 1973). Pulse amplitudes up to 50 V were tested to be consistent with experimental protocol but both sensory and motor activation would reach 100% using higher voltages. Additionally, smaller diameters required a higher voltage to activate than larger diameters (Fig. 10B), as expected (W. M. Grill 2004). Since these data were averaged across all axons in the nerve, smaller axons in closer fascicles could be activated prior to larger axons in further fascicles. For example at 20 V, 27% of the 12  $\mu$ m axons were activated while 83% of the 14  $\mu$ m axons were activated.

At lower voltages, more axons in fascicles closest to the electrodes were activated than in the further fascicles as expected (Fig. 11A). In each nerve cross-section, there were three discrete groups of fascicles that had similar activation patterns (Fig. 11B). This suggests that selectivity by a small group of fascicles is possible using surface electrical stimulation and supports reports of sensation in small portions of the hand without muscle contraction (Forst et al. 2015).

Linear regression models were created to predict percent activation of the nerve and percent activation of a fascicle based on the input variables of stimulation voltage, axon or fascicle diameter, axon type and distance from the electrode. The regression models were also used to determine which variables had significant contribution to the overall activation. These linear regression models were able to explain between 80 and 93% of the variability in the data.

Predictions of whole nerve activation with a linear regression model were only able to explain 84% of the variability. This level of accuracy was obtained by the inclusion of all two and three way interactions. The regression model found that the input variables of axon diameter, stimulation voltage and type of axon (sensory or motor) were all significant contributors (p<0.01), as would be expected from our understanding of the system. However, given the accuracy of the regression model, it could not be used to replace the simulations described above.

Another linear regression model was created to predict the percent of axons activated in a fascicle, based on the distance of the fascicle from the electrode and the cube root of the voltage with 93% of the variability accounted for ( $R^2$ =0.93). The radius of the fascicle was found to have a smaller impact on activation (p=0.08 versus p<2<sup>-16</sup> for the other factors) and was not included in this model. When this fascicular model (see Eqn. 1) was used to predict whole nerve activation given the location of the 10 fascicles in cross section C from Fig. 2, 98% of the variability could be accounted for (Fig. 12). This suggests that a linear regression model could be used to generate data

for different nerve cross-sectional arrangements which would decrease the model runtime for future configurations with the same electrode parameters.

 $FasciclePercentActivated = -29.2 - 11.2 * (Distance to Electrode) + 59.3 * \sqrt[3]{Voltage}$ (1)

#### **4 DISCUSSION**

An anatomically-based finite element model of the arm in combination with new motor and sensory axon models were used to predict axon activation in the median nerve. The axon models could reproduce experimental results for conduction velocity, strength-duration curves and activation threshold. Differences in action potential shape between the motor and sensory models reflected differences found in experimental recordings. The models predicted a lower threshold for sensory axons than motor axons of the same diameter, allowing a range of sensory axons to be activated before any motor axons.

#### 4.1 Arm Model

Most prior research looking at nerve activation in the arm ignores the gross anatomy and simplifies the arm into a series of tissue layers (Goffredo et al. 2014; Keller and Kuhn 2008; Kuhn et al. 2009; Panescu et al. 1994; Sha et al. 2008). While still involving significant simplification, the two cross section model does account for much of the anatomical details that occur in the human arm directly under the electrodes. The size of muscles, amount of fat, diameter of the arm, and exact location of nerves varies across individuals but this model predicts activation voltages that are quite similar to those found experimentally (sensation threshold of 15-35V) (Forst et al. 2015).

#### 4.2 Axon Models

Models that captured the differences between motor and sensory axons were needed to predict the differential activation of these fibers in the nerve. It has long been known that motor and sensory fibers respond differently to electrical stimulation. Early studies suggested that there were differences in their responses to pulse duration where sensory axons had a lower threshold at longer pulse durations and motor axons had a lower threshold at shorter pulse durations (Erlanger and Blair 1938; Veale et al. 1973). More recent findings did not confirm this difference but did confirm that sensory axons had a lower threshold than motor axons (Forst et al. 2015; Mogyoros et al. 1996; Panizza et al. 1994). The new models presented in this study were built using membrane properties derived from physiological data and/or validated in prior modeling studies. These new models also show that sensory axons have a lower activation threshold than motor axons for the same diameter.

The chronaxie times calculated from the strength-duration curves were found to be higher for sensory axons than for motor axons, consistent with experimental results (Bostock and Rothwell 1997; Mogyoros et al. 1996; Panizza et al. 1994). However, the chronaxie time for the sensory axon model reported here was slightly below the range reported experimentally (230  $\mu$ s vs. 300-700  $\mu$ s). This lower chronaxie time can also be seen in Fig. 7B in the differences in the curve of the model data compared to the experimental data, even though the model stayed within the experimental range. Because of this slight difference, threshold may be underestimated at lower pulse durations. Since our whole nerve experiments were performed at 100 $\mu$ s, the predictions reported here should be minimally affected by this difference.

Differences were seen between the models and experimental data in the membrane voltage following the action potential. Even though the time durations of the model action potentials did not follow the experimental voltage, the changes in action potential shape that arose as motor parameters were converted to sensory values mirrored the differences between experimental recordings from motor and sensory axons. This suggests that the differences reported by Howells are appropriately converting the motor axon to a sensory axon. The inaccuracies during the afterpotential likely limit the use of these models to low frequency stimulation situations, where repeated stimuli only occur once the afterpotential would have concluded. Since the afterpotential has been reported to last up to 100 ms (C. McIntyre et al. 2002), stimulation at or above 10 Hz should be acceptable.

#### 4.3 Sensitivity Analysis

<u>Fast Na<sup>+</sup> conductance</u>: The same value was used for fast Na<sup>+</sup> channel conductance in both the motor and sensory models as was suggested in the Howells model (Howells et al. 2012). Since the conductance was the same in both models and had a similar

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effect on threshold (from the sensitivity analysis), the actual choice of value was less important so the value from the MRG model was used. Any variability due to this choice should be similar between the two models.

<u>HCN conductance</u>: A value for HCN channel conductance could not be found in literature in the units of conductance per unit area, and the surface area of the internode used in the Howells model was not specified to allow the conversion of the value for use in the full axon model. A range of values were tested, and it was found that when the HCN conductance was too high, the axon fired spontaneously. Therefore, conductance values were investigated in the range that did not produce spontaneous firing in either the sensory or motor axon models. The ratio between the conductance of motor and sensory axons given in the Howells model (Howells et al. 2012) was maintained as values were altered for testing, because the focus was on the accuracy of the comparison between motor and sensory axons. Pairs of values fitting the ratio were tested in the motor and sensory models to find the pair that made the steady-state voltage in each model closest to the resting potential given for motor and sensory axons in Howells. These became the nominal values for HCN conductance: 2.232 mS/cm<sup>2</sup> for motor and 3.102 mS/cm<sup>2</sup> for sensory.

<u>Leak conductances</u>: The effect of altering leak conductance was slightly different based on the location of the channel. Doubling or halving the leak conductance in the MYSA had the greatest effect on threshold  $(15 \pm 9\%)$  of threshold), but in the node or FLUT and STIN this also altered the threshold by about 1 volt ( $4.8 \pm 1\%$  of threshold). The leak conductance in the node of the motor axon was retained from the MRG model. This was converted to an appropriate value for the sensory model using the ratio of sensory to motor nodal leak conductances reported in the Howells model. The internode leak was calculated based on the report that it had 35 times lower conductance than the node (Roper and Schwarz 1989). This process found leak conductance values in the internode of 0.2 mS/cm<sup>2</sup> for motor and 0.1716 mS/cm<sup>2</sup> for sensory. If the sensory value had been found by instead multiplying the motor internodal value by the Howells ratio of sensory to motor, the value would have been 0.1825 mS/cm<sup>2</sup>. This was a 6.3% increase in the parameter, and since this is much less than the 100% increase from the sensitivity analysis, the choice to maintain the exact ratio of node to internode, rather than the exact ratio of motor to sensory in the internode, should not have had a large effect on the final threshold. Since the nodal to internodal ratio was determined from experimental results, this method was preferable to specifying internodal conductance using model predictions. The use of these values for all internodal segments originally caused the axon models to fire spontaneously, so the leak conductance of the MYSA was increased in both the motor and sensory models to match the ratio between the conductance of MYSA and the conductance of FLUT and STIN in the MRG model. This eliminated the spontaneous firing and still maintained reported relationships between motor and sensory axons.

The leak conductance values affected the threshold by at most five volts when they were altered drastically by doubling or halving the chosen value in an axon with 12  $\mu$ m diameter. For an axon of this size, the difference in threshold between motor and sensory axons was about twelve volts. The basic model predictions can therefore be considered fairly resilient to variability in individual parameters. Additionally, since all of the sensory and motor conductance values were related by a fixed ratio from Howells et al., a change in one model would lead to a proportional change in the other. Since the sensitivity analysis shows that parameters have similar effects in both models, the comparison of motor and sensory thresholds is also resilient to parameter adjustments.

#### 4.4 Whole Nerve Activation

At each voltage, larger axons were recruited at higher percentages than smaller axons, as expected. However, since axons of different diameters were distributed throughout the nerve, smaller axons were activated at voltages that did not fully activate the larger axons. For example some 13  $\mu$ m and 14  $\mu$ m fibers were activated at 15 V, when 50% of the 15  $\mu$ m fibers were activated. This is similar to results reported using a simpler concentric tissue model of the arm (Goffredo et al. 2014).

Fascicular diameter was not found to be a significant contributor to axon activation (p=0.08 and a change in  $R^2$  of 0.07%). Since the perineurium was set as a percentage of the fascicle diameter, prior studies have found that the activation threshold increases with larger fascicles. For example, change in percent activation of around 15% for a similar range of fascicle diameters as in the present study has been reported (Grinberg

et al. 2008). It is likely that the greater distance from the electrodes and the significant amount of tissue for the current to travel through decreased the effect of the varying thickness of the perineurium.

#### 4.5 Additional Limitations and Implications

Electrostatic simulations like the ones performed here have previously been successful at predicting activation using nerve-based electrodes (Schiefer et al. 2008). This solution method neglects the effect of tissue capacitance which will affect the shape and amplitude of the stimulation pulses within the tissue. Other models of surface stimulation using simplified geometry have used both electrostatic (Kuhn et al. 2010) and time-domain simulations which take into account capacitive effects of the different tissue types (Dorgan and Reilly 1999; Kuhn et al. 2009). The specific contribution of capacitive tissue properties in a detailed tissue model needs further investigation. Because the simulations neglect the effect of capacitance, other details of the model are less critical. For instance, the hydrogel layer of the electrode-skin interface was not included but a major effect of this layer is due to its capacitance. The overall effects of these FEM limitations on the electric field should be the same for all axons in the nerve. Therefore, the analysis and conclusions drawn about the relative activation of different axons based on their diameter, location or whether they were sensory or motor axons should be valid.

Consistent responses are difficult to obtain using surface electrical stimulation due to variable electrode placement, skin movement and physiological variables that effect tissue conductance. A viable clinical system must be able to overcome these challenges. The models presented here will be used to predict the function of an electrode array that would be placed over the elbow to achieve activation of multiple nerve locations across a range of anatomical variations. The model will also be used to design an algorithm that allows real-time adjustment of stimulation parameters based on user feedback to change the location of the evoked sensation. The model-optimized design will then be tested in human subjects to validate its effectiveness.

In addition, the sensory and motor axon models will play a vital role in the future development of sensory feedback systems for people with limb amputations. These models can be used to predict responses in other stimulating conditions, such as when using nerve cuff or intraneural electrodes. The ability to explore different stimulation methods to target motor or sensory axons will be invaluable.

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# FIGURES



Fig. 1 The Modeled Arm, in ANSYS Maxwell. The electrodes are placed over the elbow



**Fig. 2** Nerve cross-sections. (a) Single fascicle nerve used for initial testing of axon models. (b) Median nerve cross section from the elbow of a human cadaver. (c-e) Modeled versions of the median nerve with randomly arranged fascicles



Internodal channels Nodal channels **Fig. 3** Overview of the Models. (a) Overall structure of the axon model. Between each node of Ranvier are two MYSA segments, two FLUT segments, and six STIN segments. Together, these segments make up the internode, which is sheathed in myelin. The model contains 161 nodes and 160 internodes. (b) The ion channels modeled as voltagedependent resistors. The internodal segments contain fast K<sup>+</sup>, slow K<sup>+</sup>, and HCN channels, with leak resistance and internodal capacitance. The node contains fast K<sup>+</sup>, slow K<sup>+</sup>, fast Na<sup>+</sup>, persistent Na<sup>+</sup>, and leak channels, with nodal capacitance. Also represented are the conductance  $G_m$  and capacitance  $C_m$  of the myelin, the axoplasmic conductance  $G_a$ , and the periaxonal conductance  $G_p$ 



#### Axon Diameter (µm)

**Fig. 4** Distribution of Axon Diameters in the Median Nerve. Blue bars are the distribution reported by Buchthal with the height of the bar listed at the base (Buchthal and Rosenfalck 1966). The orange points show the actual distribution that resulted from the random assignment of axon diameters (error bars denote one standard deviation). Note that axons with diameters less than 6  $\mu$ m were not included because they were not activated by voltages within the experimental range of 1-50 V



Fig. 5 Comparison of motor and sensory thresholds for different fiber diameters



**Fig. 6** The relationship between conduction velocity and fiber diameter in the model closely resembled the relationship measured in cats. The dotted line was obtained from the equation fit to the group I afferent fibers and adjusted for the assumed 20% shrinkage reported in the study (I A Boyd and Kalu 1979)



**Fig. 7** Normalized strength-duration curves from a single motor (a) and sensory (b) axon in the singular fasicular median nerve. The grey areas were drawn using the mean and standard deviation reported experimentally (Panizza et al. 1994)







**Fig. 9** Sensitivity analysis of the effect of doubling each parameter from its nominal threshold value in motor and sensory axon models. Halving each parameter yielded similar results so these data are not included. The most influential parameters were the fast sodium channel conductance, HCN channel conductance, and leak conductance











Fig. 12 Linear regression prediction (line) compared to data from cross-section C (Fig. 2) of the median nerve (diamonds)

# Appendix A

Ion channel currents:

$$\begin{split} I_{Na} &= g_{Na} * m^3 * h * (v - E_{Na}) & (\text{Fast sodium}) \\ I_{Nap} &= g_{Nap} * p^3 * (v - E_{Na}) & (\text{Persistent sodium}) \\ I_{Ks} &= g_{Ks} * s * (v - E_K) & (\text{Slow potassium}) \\ I_{Kf} &= g_{Kf} * n^4 * (v - E_{Kf}) & (\text{Fast potassium}) \\ I_q &= g_q * q * (v - E_q) & (\text{HCN}) \\ I_{Lk} &= g_{Lk} * (v - E_{Lk}) & (\text{Leak}) \end{split}$$

where g is the conductance and E is the reversal potential.

For a given gating parameter x:

$$\frac{\mathrm{d}x}{\mathrm{d}t} = \alpha_x (1-x) - \beta_x x$$
$$\tau = \frac{1}{\alpha + \beta}$$

Where  $\alpha$  and  $\beta$  are defined as:

$$\begin{aligned} \alpha_{m}, \alpha_{p} &= Q_{10} * \frac{A * (v + B)}{1 - e^{\left[-\frac{v + B}{C}\right]}} \\ \beta_{m}, \beta_{p}, \alpha_{h} &= Q_{10} * \frac{A * \left[-(v + B)\right]}{1 - e^{\left[\frac{v + B}{C}\right]}} \\ \beta_{h} &= Q_{10} * \frac{A}{1 + e^{\left[-\frac{v + B}{C}\right]}} \\ \alpha_{s}, \beta_{s} &= Q_{10} * \frac{A}{e^{\left[\frac{v + B}{C}\right]} + 1} \\ \alpha_{n} &= Q_{10} * \frac{A * (v - B)}{1 - e^{\left[\frac{B - v}{C}\right]}} \\ \beta_{n} &= Q_{10} * \frac{A * (B - v)}{1 - e^{\left[\frac{v - B}{C}\right]}} \\ \alpha_{q} &= Q_{10} * A * e^{\left[\frac{v - B}{C}\right]} \\ \beta_{q} &= Q_{10} * \frac{A}{e^{\left[\frac{v - B}{C}\right]}} \end{aligned}$$

and  $Q_{10}$  is the temperature coefficient.

# Appendix B

# Motor Axon Parameters:

	arameters.			I				
		Node			Internode			
Voltage and time dependent parameters	A (ms-1)	B (mV)	C (mV)	A (ms-1)	B (mV)	C (mV)		
α <sub>m</sub>	1.86 <sup>i</sup>	20.4 <sup>i</sup>	10.3 <sup>i</sup>					
βm	0.086 <sup>i</sup>	25.7 <sup>i</sup>	9.16 <sup>i</sup>					
α <sub>mp</sub>	0.01 <sup>i</sup>	27 <sup>i</sup>	10.2 <sup>i</sup>					
β <sub>mp</sub>	0.00025 <sup>i</sup>	34 <sup>i</sup>	10 <sup>i</sup>					
α <sub>h</sub>	0.062 <sup>i</sup>	114.0 <sup>i</sup>	11.0 <sup>i</sup>					
β <sub>h</sub>	2.3 <sup>i</sup>	31.8 <sup>i</sup>	13.4 <sup>i</sup>					
α <sub>n</sub>	0.0462 <sup>i</sup>	-83.2 <sup>i</sup>	1.1 <sup>i</sup>	0.0462 <sup>i</sup>	-83.2 <sup>i</sup>	1.1 <sup>i</sup>		
βn	0.0824 <sup>i</sup>	-66 <sup>i</sup>	10.5 <sup>i</sup>	0.0824 <sup>i</sup>	-66 <sup>i</sup>	10.5 <sup>i</sup>		
α <sub>s</sub>	0.3 <sup>i</sup>	-27 <sup>i</sup>	-5 <sup>i</sup>	0.3 <sup>i</sup>	-27 <sup>i</sup>	-5 <sup>i</sup>		
βs	0.03 <sup>i</sup>	10 <sup>i</sup>	-1 <sup>i</sup>	0.03 <sup>i</sup>	10 <sup>i</sup>	-1 <sup>i</sup>		
α <sub>q</sub>				0.00522 <sup>ii</sup>	-107.3 <sup>ii</sup>	-12.2 <sup>iv</sup>		
βq				0.00522 <sup>ii</sup>	-107.3 <sup>ii</sup>	-12.2 <sup>iv</sup>		
Channel Conductances		(mS cm <sup>-2</sup> )			(mS cm <sup>-2</sup> )			
Persistent Sodium		10 <sup>i</sup>						
Fast Sodium	3000 <sup>i</sup>							
Slow Potassium	80 <sup>i</sup>			2.581 <sup>iv</sup>				
Fast Potassium	25.68 <sup>iii</sup>			150.74 (MYSA) <sup>iv</sup> , 25.68 (FLUT, STIN) <sup>iv</sup>				
Leak		7 <sup>i</sup>			2 (MYSA) <sup>v</sup> , 0.2 (FLUT, STIN) <sup>iv</sup>			
HCN					2.232 <sup>iii</sup>			
Reversal Potentials		(mV)			(mV)			
Sodium		50.0 <sup>i</sup>						
Slow		-90.0 <sup>i</sup>			-90.0 <sup>i</sup>			
Potassium								
Fast		-90.0			-90.0			
Potassium								
Leak	-90.0'			-90.0'				
HCN				-54.9 <sup>vi</sup>				

## **Sensory Axon Parameters**

	Node			Internode			
Voltage and time dependent parameters	A (ms-1)	B (mV)	C (mV)	A (ms <sup>-1</sup> )	B (mV)	C (mV)	
αm	1.77753 <sup>vii</sup>	20.1795 <sup>vii</sup>	10.3 <sup>viii</sup>				
βm	0.0823 <sup>vii</sup>	25.4746 <sup>vii</sup>	9.16 <sup>viii</sup>				
αmp	0.00957 <sup>vii</sup>	26.852 <sup>vii</sup>	10.2 <sup>viii</sup>				
βmp	0.00024 <sup>vii</sup>	33.8333 <sup>vii</sup>	10 <sup>viii</sup>				
αh	0.075286 <sup>vii</sup>	112.7124 <sup>vii</sup>	8.391 <sup>vii</sup>				
βh	2.8083 <sup>vii</sup>	30.5435 <sup>vii</sup>	10.2263 <sup>vii</sup>				
αn	0.0462 <sup>viii</sup>	-83.2 <sup>viii</sup>	1.1 <sup>∨iii</sup>	0.0462 <sup>viii</sup>	-83.2 <sup>viii</sup>	1.1 <sup>viii</sup>	
βn	0.0824 <sup>viii</sup>	-66 <sup>viii</sup>	10.5 <sup>viii</sup>	0.0824 <sup>viii</sup>	-66 <sup>viii</sup>	10.5 <sup>viii</sup>	
as	0.3 <sup>viii</sup>	-27 <sup>viii</sup>	-5 <sup>∨iii</sup>	0.3 <sup>viii</sup>	-27 <sup>viii</sup>	-5 <sup>viii</sup>	
βs	0.03 <sup>viii</sup>	10 <sup>viii</sup>	-1 <sup>∨iii</sup>	0.03 <sup>viii</sup>	10 <sup>viii</sup>	-1 <sup>∨iii</sup>	
αq				0.00522 <sup>ii</sup>	-94.2 <sup>ii</sup>	-12.2 <sup>ii</sup>	
βq				0.00522 <sup>ii</sup>	-94.2 <sup>ii</sup>	-12.2 <sup>ii</sup>	
Channel Conductances		(mS cm <sup>-2</sup> )			(mS cm <sup>-2</sup> )		
Persistent Sodium		10 <sup>viii</sup>					
Fast Sodium		3000 <sup>viii</sup>					
Slow Potassium	41.06 <sup>vii</sup>			1.324 <sup>iv</sup>			
Fast Potassium	27.37 <sup>iii</sup>			164.2 (MYSA) <sup>iv</sup> , 27.37 (FLUT,STIN) <sup>iv</sup>			
Leak	6.005 <sup>vii</sup>			1.716 (MYSA) <sup>v</sup> , 0.1716 (FLUT,STIN) <sup>iv</sup>			
HCN				3.102 <sup>iii</sup>			
Reversal Potentials	(mV)			(mV)			
Sodium	50.0 <sup>viii</sup>						
Slow Potassium		-90.0 <sup>viii</sup>			-90.0 <sup>viii</sup>		
Fast Potassium	-90.0 <sup>viii</sup>			-90.0 <sup>viii</sup>			
Leak	-90.0 <sup>viii</sup>			-90.0 <sup>viii</sup>			
HCN				-54.9 <sup>vi</sup>			

<sup>i</sup> McIntyre, et al., 2002

<sup>ii</sup> Howells, et al., 2012, Table 2

<sup>iv</sup> Converted from corresponding nodal value using ratios found by Röper and Schwarz, 1989

<sup>v</sup> Converted from corresponding flut/stin value using ratio used by McIntyre, et al., 2002.

vi Calculated using Ex equation and concentrations reported by Howells 2012

vii Converted from the corresponding motor value using ratio found in Howells, et al., 2012.

viii Howells, et al. 2012 indicates no difference between motor and sensory axons for this parameter

iii See text.